

Analytic Modelling of the Long-

term Evolution of Orbital Debris

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Debris modelling



- Debris evolution modelling often uses numerical simulation (eg. MASTER)
- Can simple analytical models provide useful insights into debris evolution?
- Present two simple models for population dynamics using ODE and PDE







Particle-in-a-box model



- Simple model to capture key process in evolution of orbit debris population
- Model no. of debris objects N with non-linear first order evolution equation
- Define debris deposition rate A, removal rate B and collisional growth rate C

$$\frac{dN}{dt} = A + BN + CN^{2}$$

$$\dot{N} = 0$$

$$N_{1,2} = \frac{-B \pm \sqrt{B^{2} - 4AC}}{2C}$$

Talent, D: 'Analytical model for orbital debris environmental management'. J. Spacecraft and Rockets, Vol. 29, No. 4, July-August 1992

Stable and unstable regiemes



- Equilibrium condition yields quadratic with 2 distinct roots (debris end states)
- Discriminant of quadratic is a measure of difference between sinks/sources
- Therefore have 3 possible conditions . . .

$$q = B^2 - 4AC$$
$$= Sinks - Sources$$

$$q > 0 \Rightarrow Sinks > Sources \Rightarrow STABLE$$

 $q = 0 \Rightarrow Sinks = Sources \Rightarrow THRESHOLD$
 $q < 0 \Rightarrow Sinks < Sources \Rightarrow UNSTABLE$









Continuum PDE model



- Assume that debris population is a continuum (really a collisionless fluid)
- Debris population is therefore described by the debris number density n
- For continuum problems can use the tools of *partial differential equations*

McInnes, C.R.: 'An analytical model for the catastrophic production of orbital debris', European Space Agency Journal, Vol. 17, No. 4, pp. 293-305, 1993. JOURNAL OF GUIDANCE, CONTROL, AND DYNAMICS Vol. 23, No. 2, March-April 2000

Simple Analytic Model of the Long-Term Evolution of Nanosatellite Constellations

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McInnes, C.R.: 'A simple analytic model of the long term evolution of nanosatellite constellations', Journal of Guidance, Control and Dynamics, Vol. 23, No. 2, pp. 332-338, 2000.

The long-term evolution of a large constellation of nanosatellites is investigated using closed-form analytical methods. A set of partial differential equations is derived, the solution to which provides the evolution of the mean spatial number density of the constellation under the action of air drag, on-orbit satellite failures, and the deposition of new satellites into the constellation. These solutions give insight into the global dynamics and long-term evolution of large constellations of nanosatellites and display some interesting physical features. In particular, asymptotic solutions provided the steady-state distribution of nanosatellites and an estimate of the required rate of deposition of new nanosatellites to maintain the constellation.

Population dynamics



- Assume the debris density n is now a function of orbit radius r and time t
- Assume there exist source terms (new objects) and sink terms (sweepers)
- Also, the inflow due to air drag a radial speed v_r (r) which is a function of r

$$\frac{\partial n(r,t)}{\partial t} + \frac{1}{r} \frac{\partial}{\partial r} (rv_r(r)n(r,t)) = \dot{n}^+(r,t) - \dot{n}^-(r,t)$$

We'll derive this shortly. . . .





Evolution timescales



- Assuming that debris population described as a function of orbit radius only
- Could model entire population as a symmetric sphere with radial structure
- Could model fragmentation events after a uniform torus has been formed







Particle dynamics



- Assume that motion of debris is quasi-circular so local Keplerian motion
- For 2D disk assume that motion is entirely planar (the torus is flat)
- Radial inflow due to air drag a function of orbit radius r and ballistic coeff B

$$v_{r} = -f(r, B)$$

$$v_{\theta} = \sqrt{\frac{\mu}{r^{3}}}$$

$$v_{z} \sim 0$$
Inflow of debris due to air drag





Air drag



- Assume isothermal exponential atmosphere of density *r* and scale height *H*
- Determine inflow speed from the work done by air drag on the debris particle
- For quasi-circular motion obtain inflow speed of debris (radial shearing ...)

$$a = \frac{1}{2} B\rho(r) v^{2} \quad , \quad \rho(r) = \rho_{o} \exp\left(-\frac{r-R}{H}\right)$$
$$\longrightarrow v_{r}(r) = -\sqrt{\mu r} B\rho_{o} \exp\left(-\frac{r-R}{H}\right)$$

Debris inflow



- Consider inflow of debris through control element at radius r and of width Δr
- In control volume/area $2\pi r \Delta r$ have a total number of particles $2\pi r \Delta r.n(r,t)$
- Need to conserve total number of particles remember $v_r(r)$ is negative!

$$\begin{aligned} \frac{\partial}{\partial t} (2\pi r \Delta r n(r,t)) &= v_r(r) 2\pi r n(r,t) & Flow in \\ &- v_r(r + \Delta r) 2\pi (r + \Delta r) n(r + \Delta r,t) & Flow out \\ &+ 2\pi r \Delta r (\dot{n}^+(r,t) - \dot{n}^-(r,t)) & Deposition-Sweeper \end{aligned}$$





Continuity equation

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- Now take the limit as control element width $\Delta r \rightarrow 0$ to obtain continuity PDE
- Solution describes time evolution of radial structure of the debris population
- Since we have a PDE need to provide some initial data n(r,0) defined at t=0

$$\frac{\partial n(r,t)}{\partial t} + \frac{1}{r} \frac{\partial}{\partial r} (rv_r(r)n(r,t)) = \dot{n}^+(r,t) - \dot{n}^-(r,t)$$

$$\rightarrow \frac{\partial n(r,t)}{\partial t} + \frac{\partial n(r,t)}{\partial r} v_r(r) + n(r,t) \left[\frac{v_r'(r)}{v_r(r)} + \frac{1}{r} \right] v_r(r) = \dot{n}^+(r) - \dot{n}^-(r)$$

Solving the continuity equation



- Solution to ODE has arbitrary constant, solution to PDE arbitrary function . . .
- PDE is linear, so can in principle solve using the method of characteristics
- Separate single PDE into two ODEs if can find characteristics can solve

$$-\left[-n(r,t)\left[\frac{v_r'(r)}{v_r(r)} + \frac{1}{r}\right]v_r(r) + \dot{n}^+(r) - \dot{n}^-(r)\right]^{-1}dn = v_r(r)^{-1}dr = dt$$

$$\frac{dr}{dt} = v_r(r) \quad \text{Defines family of characteristics} \dots$$

$$\frac{dn(r,t)}{dr} + n(r,t)\left[\frac{v_r'(r)}{v_r(r)} + \frac{1}{r}\right] = \frac{1}{v_r(r)}\left[\dot{n}^+(r) - \dot{n}^-(r)\right]$$

Solving the characteristic equation



- Can see that physically, the characteristic curve is the inwards flow of debris
- Integrate to obtain function relating orbit radius and time the characteristics
- Needs this to obtain the general solution to the continuity equation PDE later

$$\frac{dr}{dt} = v_r(r) = -\sqrt{\mu r} B\rho_o \exp\left(-\frac{r-R}{H}\right)$$

$$\Rightarrow \frac{1}{\alpha} \int \frac{\exp(r/H)}{\sqrt{r}} dr + t = -C \quad , \quad \alpha = \sqrt{\mu} B\rho_o \exp(R/H)$$

$$\exp(r/H) + \frac{\alpha\sqrt{R}}{H} t = \tilde{C} \quad , \quad \tilde{C} = -\frac{\alpha\sqrt{R}}{H} C$$



Debris evolution



- Assume that there is no deposition of new debris particles, or debris removal
- Simply ODE need to solve to obtain the debris density distribution function
- Add arbitrary function of characteristic equation determine from initial data

$$\frac{dn(r,t)}{dr} + n(r,t) \left[\frac{v_r'(r)}{v_r(r)} + \frac{1}{r} \right] = 0$$

$$\Rightarrow ln\{n(r,t)\} = ln\{rv_r(r)\}^{-1} + \Psi(G(r,t))$$





Asymptotic distribution



- If we now have deposition of new debris particles then steady-state possible
- Deposition of new particles balanced by the removal of debris by air drag
- Find that the asymptotic solution of the continuity PDE given by an integral

$$n_{\infty}(r) = \frac{1}{r^2 v_r(r)} \int r^2 \dot{n}^+(r) dr + D$$

Debris sweepers



- Now assume we have a debris sweeper device active on a fixed circular orbit
- Define using a Dirac delta function so device is active at single orbit radius
- Assume the sweeper removes fixed fraction of debris inflow passing it's orbit

$$\dot{n}^{-}(r,t) = -2\pi r v_{r}(r) n(r,t) \lambda \delta(r-\bar{r})$$





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